

Performance Investigation of a Dual-Source Heat Pump for a Swine Nursery Barn in Northern Italy

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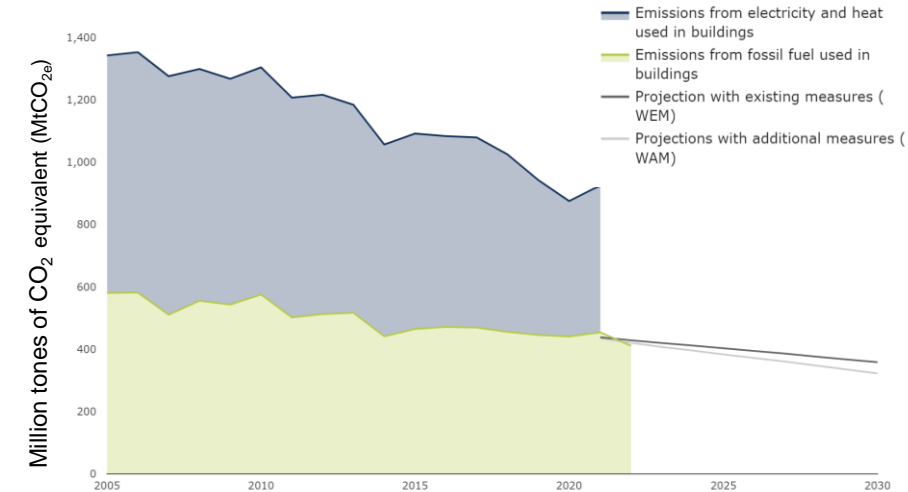
Presentation Outline

- Introduction
- System design and description
- Methodology
- Experimental results
- Seasonal Coefficient Of Performance
- Digital capacity operation
- Conclusions

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General Context



European Environment Agency (EEA). Greenhouse gas emissions from energy use in buildings in Europe. 24 Oct 2023:
<https://www.eea.europa.eu/en/analysis/indicators/greenhouse-gas-emissions-from-energy>

- **Buildings contribute to ~40% of global carbon emissions – decarbonizing heating is crucial.**
- **Heat pumps (HPs) are efficient electric devices gaining momentum due to government initiatives to more sustainable solution.**

Focusing on livestock buildings...

- **Major source of greenhouse gas (GHG) emissions, especially intensive livestock and husbandry facilities due to:**

- High energy consumption
- Extensive use of fossil fuels



Replace current technologies with reliable RES solutions to consume less energy and improve the thermal conditions

Introduction

Scope of the work

Replacement of a 35 kW LNG boiler of a nursery barn

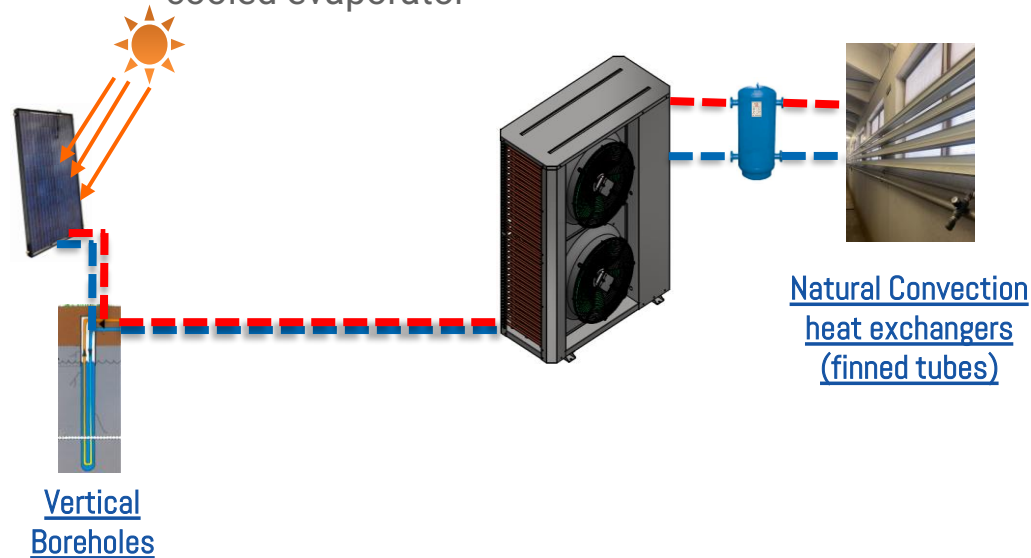


Nursery Barn in Northern Italy

With



- Multisource (air/water) heat pump with **hybrid** operation
- Medium temperatures (up to 45 oC) for higher COP
- Sources: Geothermal and solar for water | Air-cooled evaporator



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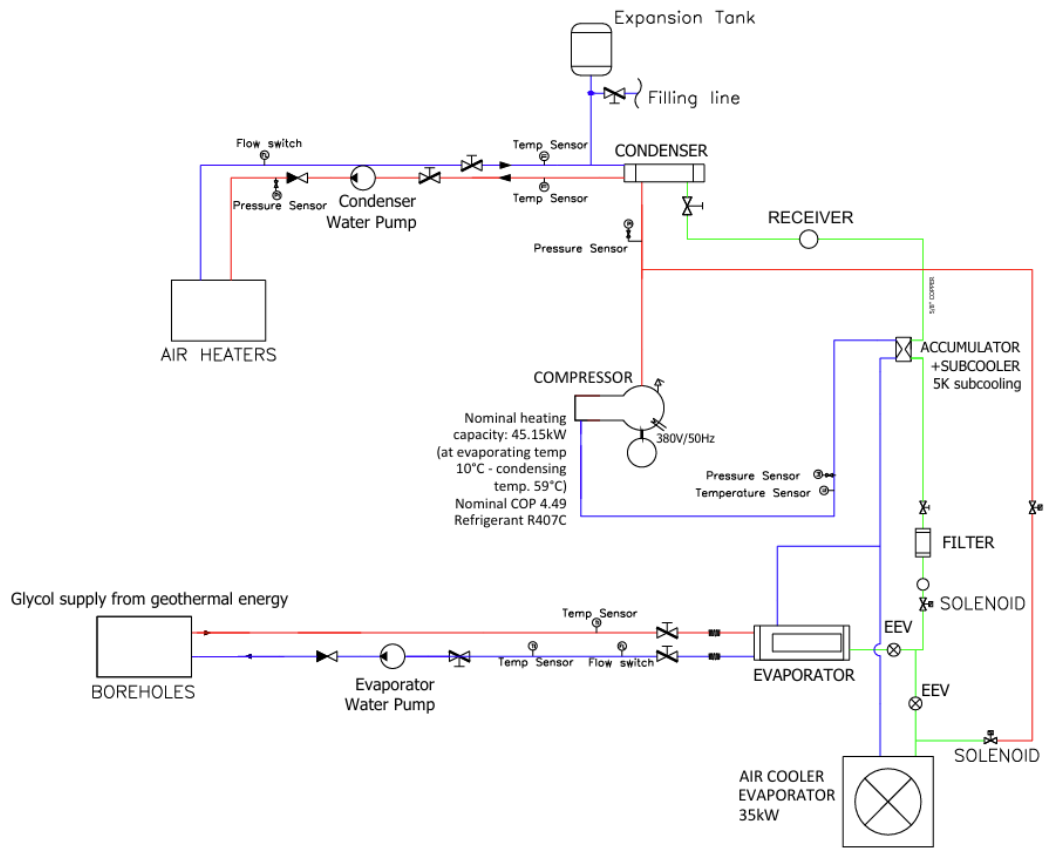
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System design and description

Cycle Design Parameters

- Refrigerant R407C
- Condensing temperature: 58 °C
- Evaporating temperature: 13 °C
- Superheat / subcooling: 10 K / 5 K
- Pinch point: 3 K
- Specified water flowrates

Water/ glycol flow	Temperature (°C)	Flowrate (m3/h)
Evaporator (in / out)	20 / 15	6.4
Condenser (in / out)	45 / 55	3.9



System design and description

Plate HEXs used for efficient heat transfer:

Heat exchanger	Model	Plates	Surface (m ²)
Condenser	B85H	100	5.88
Evaporator	B80H	80	4.68



Design conditions

DUTY REQUIREMENTS		Side 1	Side 2
Fluid		R407C	Water
Flow type	Condenser	Inner	Outer
Circuit			
Heat load	kW	45,15	
Inlet vapor quality		1,000	
Outlet vapor quality		0,000	
Inlet temperature	°C	70,00	45,00
Condensation temperature (dew)	°C	58,00	
Subcooling	K	2,00	
Outlet temperature	°C	51,83	55,00

DUTY REQUIREMENTS		Side 1	Side 2
Fluid		R407C	Ethylene Glycol - Water (20,0 mass%)
Flow type	Evaporator	Inner	Outer
Circuit			
Heat load	kW	35,10	
Subcooled liq. temp.	°C	43,00	
Inlet vapor quality		0,268	
Outlet vapor quality		1,000	
Inlet temperature	°C	9,00	20,00
Evaporation temperature (dew)	°C	13,00	
Superheating	K	5,00	
Outlet temperature	°C	18,00	15,00

System design and description

System design

Air heated evaporator

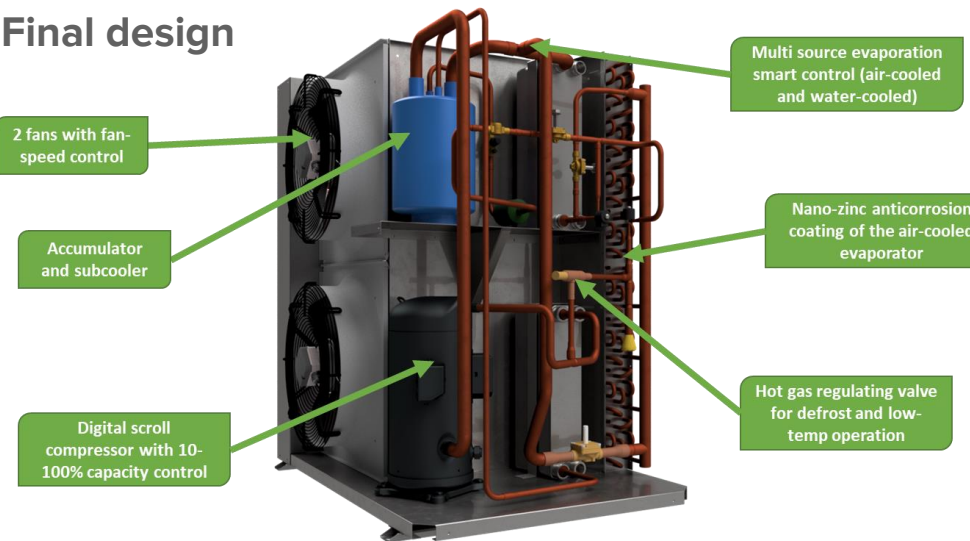
Air of 0°C

CAPACITY OBTAINED	18677	W
EXCHANGE SURFACE	60.12	m ²
EXCHANGE GLOBAL COEFFICIENT	46	W/(m ² K)
FINS THICKNESS	0.2200	mm
COIL INSIDE VOLUME	7.3	l
TUBES OUTSIDE DIAMETER	12.7	mm
TUBES INSIDE DIAMETER	11.7	mm



System design and description

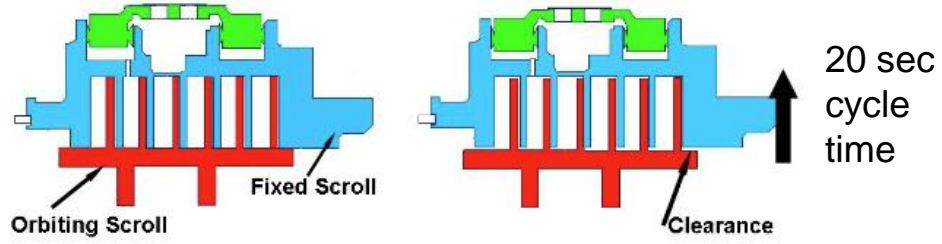
Final design



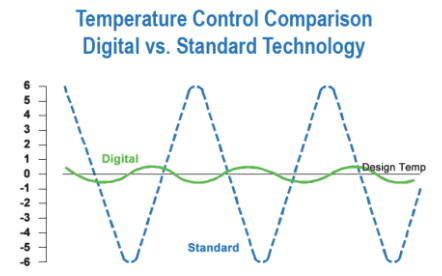
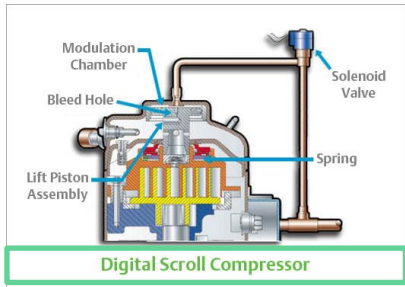
PERFORMANCE AT SPECIFIED OPERATING POINT
ZRD125KCE-TFD Data at 50 Hz

Cooling Capacity, kW	35.10
Power, kW	10.05
COP	3.49
Current at 400 V, A	17.60
Suction Mass Flow, g/s	234.00
Heating Capacity, kW	44.60
Isentropic Eff., %	72.46

Digital Scroll Technology



Compressor Selected ZRD125KCE-TFD



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Methodology

Measured values

Parameter (units)	Symbol
Electricity consumption of the compressor (net) (kW)	\dot{W}_{comp}
Electricity consumption of the auxiliary parts (kW)	\dot{W}_{aux}
Inlet temperature at the water side of the evaporator (°C)	$T_{w,evap,in}$
Outlet temperature at the water side of the evap. (°C)	$T_{w,evap,out}$
Inlet temperature at the water side of the condenser (°C)	$T_{w,cond,in}$
Outlet temperature at the water side of the cond. (°C)	$T_{w,cond,out}$
Refrigerant pressure at the discharge line (bar)	$P_{discharge}$
Refrigerant pressure at the suction line (bar)	$P_{suction}$
Water flow at the evaporator side (m ³ /h)	$\dot{V}_{w,evap}$
Water flow at the condenser side (m ³ /h)	$\dot{V}_{w,cond}$
Outdoor temperature (°C)	$T_{outdoor}$



Testing conditions

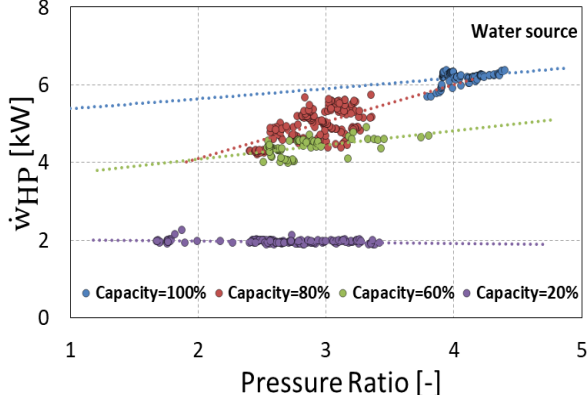
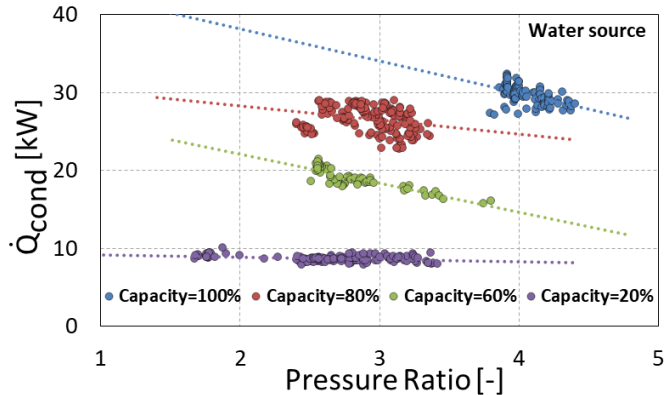
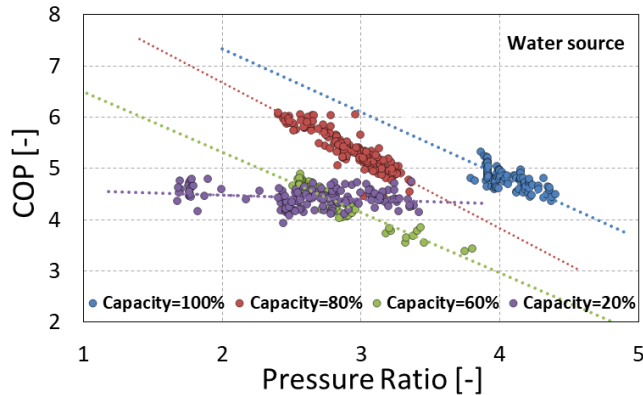
- Water temperatures at evaporator: 8 – 20 °C.
- Water temperatures at condenser: 30 – 50 °C
- Compressor capacity variation: 20 – 100%

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Experimental results – Water source

■ $T_{\text{evap,in}} \sim 10 - 20 \text{ }^\circ\text{C}$
■ $T_{\text{cond,in}} \sim 20 - 50 \text{ }^\circ\text{C}$

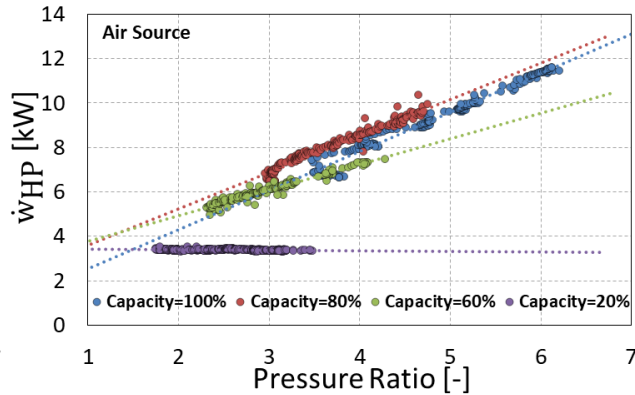
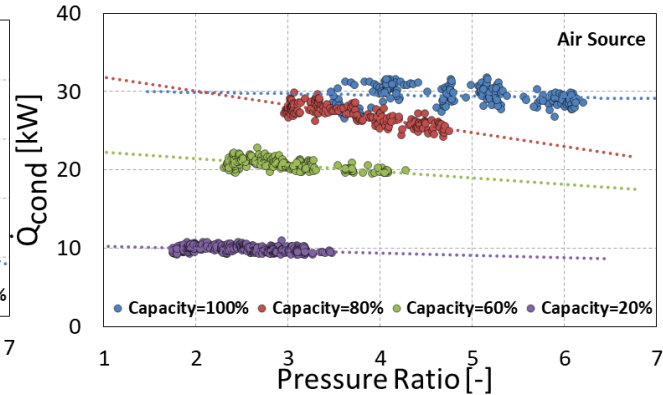
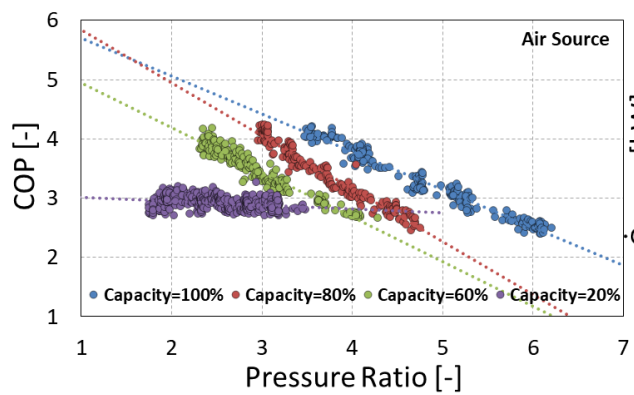


□ Condensation load and COP for capacity variation when pressure ratio is about 4:

- 100% capacity: $Q_{\text{cond}} \sim 32 \text{ kW}$, COP=5
- 80% capacity: $Q_{\text{cond}} \sim 25 \text{ kW}$, COP=3.9
- 60% capacity: $Q_{\text{cond}} \sim 15 \text{ kW}$, COP=3.0
- 20% capacity: $Q_{\text{cond}} \sim 9 \text{ kW}$, COP=4.2

Experimental results – Air source

■ $T_{\text{outdoor}} \sim 15 - 20 \text{ }^\circ\text{C}$
■ $T_{\text{cond,in}} \sim 20 - 50 \text{ }^\circ\text{C}$

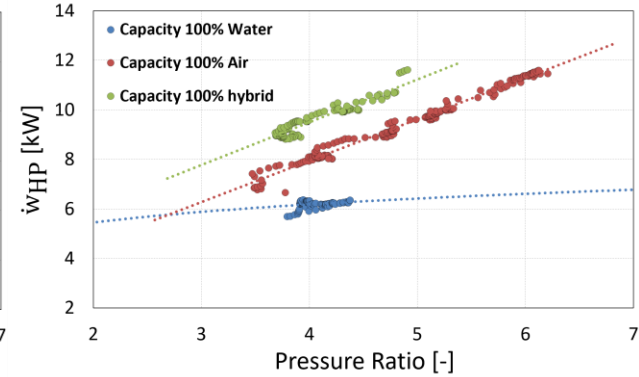
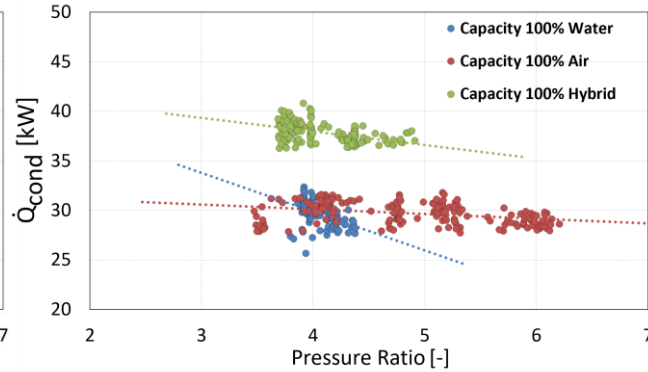
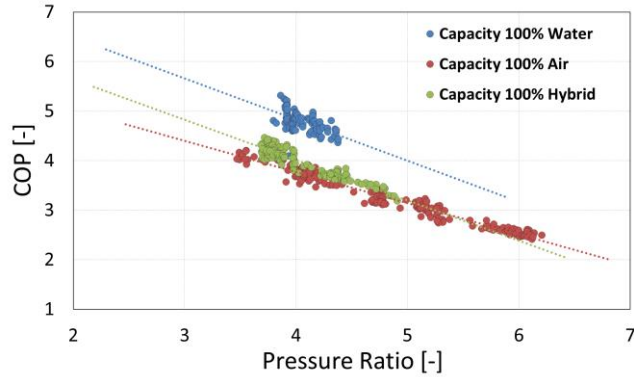


□ Condensation load and COP for capacity variation when pressure ratio 2 – 5:

- 100% capacity: $\dot{Q}_{\text{cond}} > 30 \text{ kW}$, $COP = 3.0 - 4.3$
- 80% capacity: $\dot{Q}_{\text{cond}} \sim_{25-30} \text{ kW}$, $COP = 2.3 - 4.0$
- 60% capacity: $\dot{Q}_{\text{cond}} \sim_{20} \text{ kW}$, $COP = 2.0 - 4.0$
- 20% capacity: $\dot{Q}_{\text{cond}} \sim_9 \text{ kW}$, $COP = 3.0$

Experimental results – Hybrid mode

- $T_{\text{outdoor}} \sim 15 - 20 \text{ }^\circ\text{C}$
- $T_{\text{cond,in}} \sim 20 - 50 \text{ }^\circ\text{C}$
- $T_{\text{evap,in}} \sim 10 \text{ }^\circ\text{C}$
- 100% Capacity



- High outdoor temperature during tests, results to modest enhancements in COP between hybrid and air mode: COP 4.5 (hybrid) vs 4.1 (air) in lower pressure ratios (3.5 – 4).
- Hybrid operation → Increased power consumption (fans, pumps etc.)
- Hybrid operation → 8 kWth capacity increment ($\sim 25\%$ ↑)
- Water operation → Highest COP

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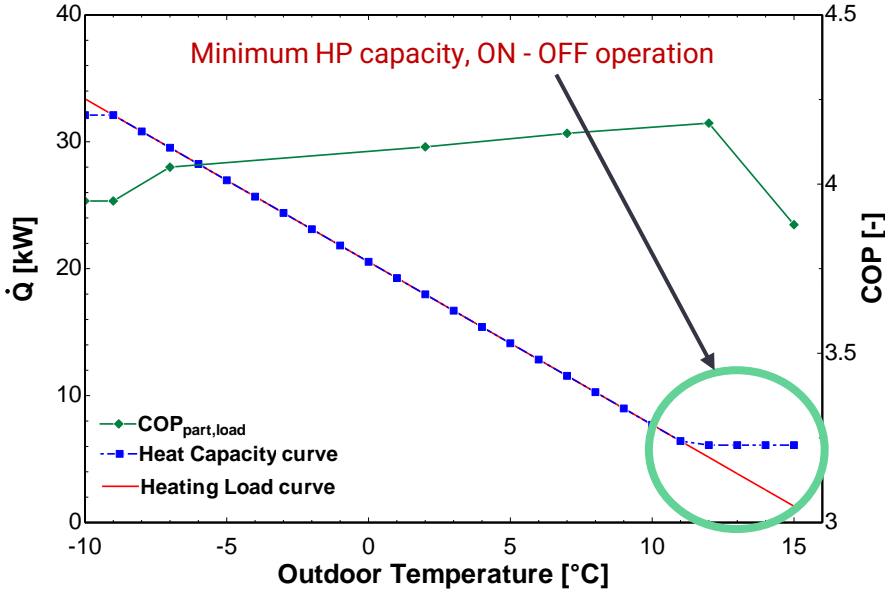
Seasonal COP

- ❖ According to EN 14825 for **water-source** (geothermal heat pumps)
- ❖ For “Average” temperature zone (Medium temp application)



Evaporator inlet: 10 °C
 Condenser outlet: 45 °C

Reference heating season		“A” Average	
Seasonal Efficiency	Reference Heating Season (EN14824), Medium temp. (Fixed outlet 45 °C)	$P_{design} (kW)$	33.38
		$SCOP$	4.08



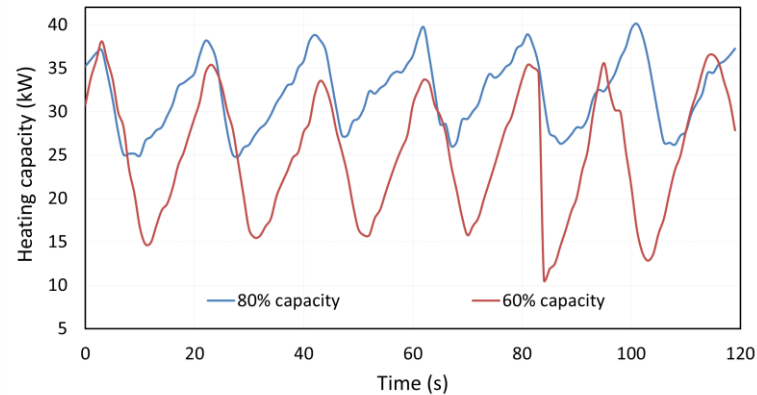
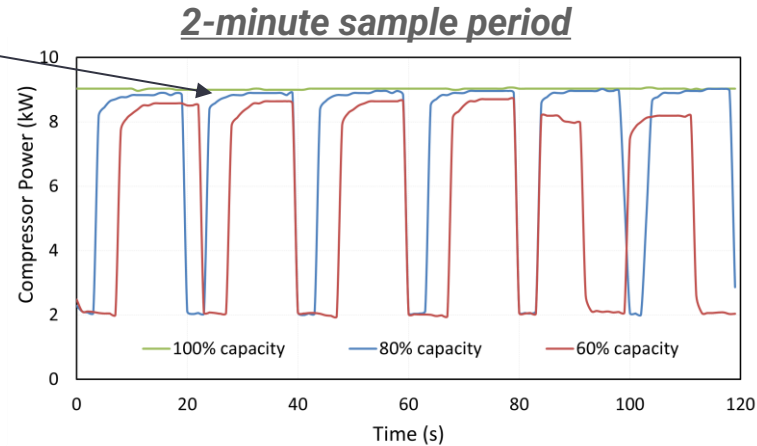
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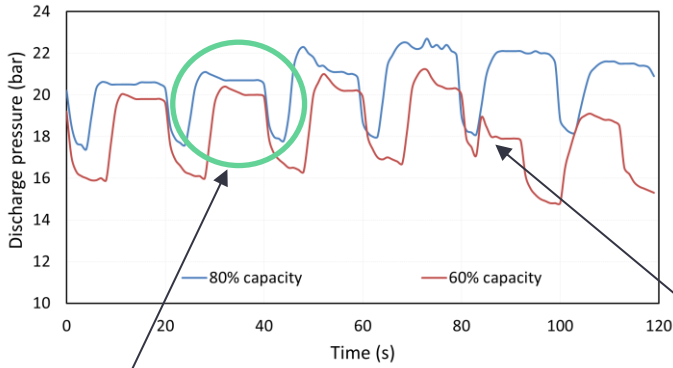
Digital capacity operation

**100% capacity
Standard scroll**

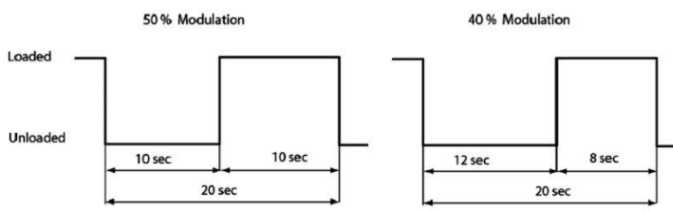
- Loaded phase: 100% capacity
- Unloaded phase: ~2 kW consump.
- 60% Capacity, 4% lower power consumption due to lower pressure ratios (loaded phase)
- 10 kW disparity between 80 and 60 % capacity in heating load



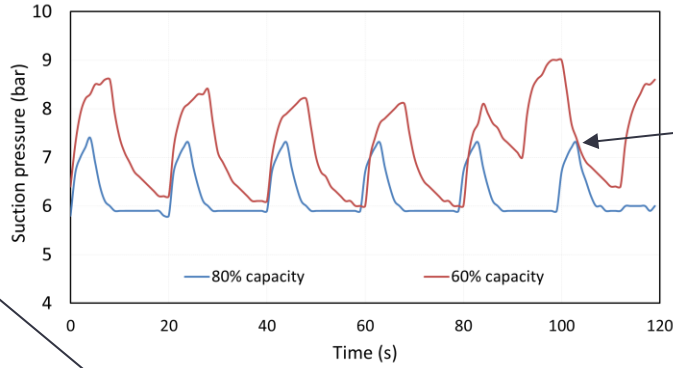
Digital capacity operation



Higher discharge pressure at 80% capacity due to ~ 5 °C higher water inlet temperature at condenser



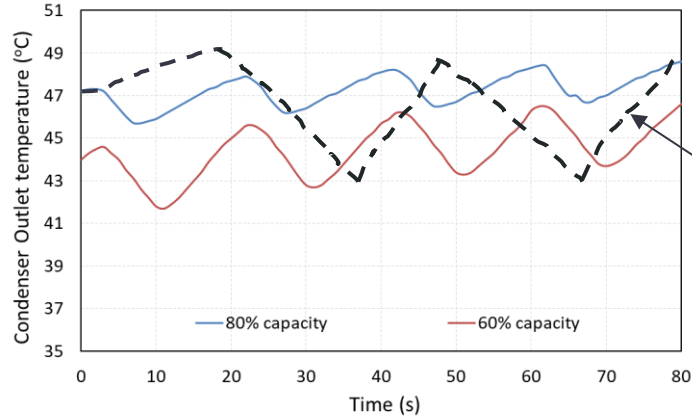
Source: www.copeland.com



Ample reheat at low loads (Suction pressure increase)

Pressure variations due to load variations

2-minute sample period



ON – OFF Scroll Compressor

Conclusions

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Conclusions

- Water source at full load → over 30 kW heating capacity with COP up to 5.
- Air source at full load → 30 kW heating capacity with COP range between 3 and 4 .
- Hybrid mode: Similar COP with air source for temperatures at 15 °C but with enhanced heating capacity (>25% compared to Water/Air mode).
- Average climate zone and Medium temperature applications result to a **SCOP of 4.08** for water source operation.
- Digital capacity modulation: Variation of heating capacity between 9 – 32 kW with COP 2 – 5. Enhanced system performance compared to standard scroll due to:
 - ✓ Precise temperature control according to the load – match capacity to demand.
 - ✓ Reduce the on – off cycling, less mechanical stress and effective lubrication.
 - ✓ Efficient part load operation, **reducing the capacity up to 80% without stopping completely.**

**Thank you for your
attention!**

Acknowledgment

This work developed in the framework of the Horizon 2020 RES4LIVE: “Energy Smart Livestock Farming towards Zero Fossil Fuel Consumption” project (www.res4live.eu) funded by the European Commission (Grant agreement No.101000785).



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